

Autonomous Car Modeling and Control summary

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Autonomous Car Modeling and Control

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- Dynamic Models
 - Car-Body Dynamics The Slow Dynamics
 - Tire Dynamics The Fast Dynamics
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 - System Equations
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 - Kinematic Lateral Speed Control Law
- Deep Autonomous Vehicle Control



Vehicle models depending on their dynamics can be classified into three major categories that we will develop below:

- Dynamic Models
- Kinematic Models
- Point Mass Models





• Dynamic Models

These models essentially describe the relationship that the vehicle has with the road. The complexity of these models results from the non linearity of the relationships between the tires and the other parts of the vehicle.





Kinematic Models

These models consist a structure of equations that describe the geometry of the vehicle, representing the behavior of the vehicle in motion and during maneuvers.



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Figure 1: Diagram of Dynamic and Kinematic Model for Autonomous Driving [TM15].



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Dynamic Models



To describe the car dynamics will be used three different frames:

- Inertial Frame: it is described as $(\mathbf{e}_X, \mathbf{e}_Y, \mathbf{e}_Z)$
- Vehicle Frame: it is described as (e_x, e_y, e_z)
- **Pneumatic or Tire Frame:** it is described as $(\mathbf{p}_{xi}, \mathbf{p}_{yi}, \mathbf{p}_{zi})$ where the *i* is associated with the wheel of the vehicle i = 1, ..., 4



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- The slow dynamics, incluse six different variables, namely the *longitudinal* V_x , *lateral* V_y and *vertical* V_z velocities and the *roll* $\dot{\theta}$, *pitch* $\dot{\phi}$ and *yaw* $\dot{\psi}$ angular velocities.
- The model inputs are the longitudinal and lateral forces F_{xi} and F_{yi} applied by the road on the different wheels *i* in the vehicle frame (or equivalently F_{xpi} and F_{ypi} in the pneumatic frame). This concept shown in Figure 3.





In the following Figure we see the Dynamics of a car which moves in a hill. We must describe the F_{aero} , which consist the air force that hits the car.



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Here we will describe the four-wheel vehicle model dynamics. Compared to the dynamic bicycle model, the slope and road-bank angle are defined, as well as the roll, pitch and vertical motions.



Artificial Intelligence & Information Analysis Lab Figure 5: Four - Wheel Dynamic Model [POL18].



The suspension force variation F_{s1} applied at wheel *i* depends on the variation of the length of the suspension $\Delta z_{s1} = z_{si} - z_{ti}$.

The normal reaction F_{zi} force applied by the road on wheel *i* is given by the following Equations. The P_r is the weight of the wheel as shown in Figure 6.

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Figure 6: The Wheel Dynamics.

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The *longitudinal* F_{xp} and *lateral* F_{yp} forces of tires are not given directly from the driver.

That is why we must describe the steering wheel actions. The tire forces generated by the gas pedal and the brake pedal.





Figure 7: Dynamics of an understeer vehicle [MKT19].





The *longitudinal* F_{xp} and *lateral* F_{yp} forces generated by the road on each tire expressed in the pneumatic frame are obtained from the following four variables:

- The longitudinal slip ratio: τ_x
- The lateral slip angle: α
- The normal reaction force of the road on the wheel: F_z
- The road friction coefficient: μ







Figure 8: The main concept of the tire dynamics.

The *Tire model* can be expressed from the following Equations:

$$F_{xp} = f_x(\tau_x, \alpha, F_z, \mu)$$

$$F_{yp} = f_x(\alpha, \tau_x, F_z, \mu)$$







The first Equation refers to the *Traction* phase while the second Equation refers to the *Braking* phase.



Now, we must describe the *lateral slip angle* a_i

It is the wheel's orientation vector *i* and the velocity vector of the same wheel as shown in Figure 10.



Figure 10: Later slip angle on the Tire Dynamic Model [POL18].





The first Equation refers to the front wheels while the second Equation refers to the rear wheels.

$$\alpha_i = \delta_f - \operatorname{atan}(\frac{V_y + l_f \dot{y}}{V_x + \epsilon l_w \dot{y}})$$

$$\alpha_i = -\operatorname{atan}(\frac{V_y + l_r \dot{y}}{V_x + \epsilon l_w \dot{y}})$$



Figure 11: The Friction circle.





Figure 12: The proposed model vehicle model [POL18]. Artificial Intelligence & Information Analysis Lab



Finally, the combination of the f principles of the *car* – *body dynamics* with a *tire model* we get a 10 Degrees of Freedom vehicle model (10 DoF).

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Kinematic Models



The Equations for this model are simpler. The kinematic vehicle model assumes that no slip occurs between the ground and the wheels, which is accurate for vehicles moving at low speeds.

In this case, the velocity directions at points F and R (V_F and V_R) are consistent with the directions of the front and rear wheels



Kinematic Models

$$\dot{X} = V_G \cos(\psi + \beta)$$

 $\dot{Y} = V_G \sin(\psi + \beta)$

 $\dot{\psi} = V_G \cos(\beta) \tan(\delta) / (l_f + l_r)$

$$\dot{V}_G = \alpha$$

$$\beta = \tan^{-1}\left(\frac{l_r}{l_f + l_r}\tan(\delta)\right)$$



Figure 13: Diagram of the four wheel Kinematic model [MWCZ19].



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Bicycle – Car Kinematic Model (VML



Because the bicycle model is often mentioned in the literature, efforts have been made to form the basis for the study and development of corresponding car models.

In the picture below we see how a bicycle model can be adapted to a kinematic vehicle model with four wheels.





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Point – Mass Models



As we described in the Introduction the **Point - Mass** models are the simplest models of a vehicle.

The latter is assimilated to a point - mass where the **control inputs** are good enough for a second order point - mass model. The accelerations in the inertial frame are the a_X and a_Y .



Point – Mass Models



The most important is that the system obtained is a linear one.

$$\dot{\xi}_{pm} = \mathbf{A}\xi_{pm} + \mathbf{B}U_{pm}$$

The second order point - mass model can described from $p_m = (X, \dot{X}, Y, \dot{Y})^T$ which is the state of the vehicle and $U_{pm} = (X, Y)^T$ which is the control input. The **A** and **B** are diagonal 4×4 and 2×2 matrices, respectively. The variables *X* and *Y* describe the **positions** of the vehicle in the inertial frame while the \dot{X} and \dot{Y} describe the **speed** of the vehicle in the inertial frame.



Point – Mass Models



As shown in Figure 15 the vehicle can move in many directions, this idea makes the model *week* and *poor* in accuracy. If we want to avoid pure lateral motion, we assume the following Equation.



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Autonomous Vehicle Control



In order to execute the reference path or trajectory from the motion planning system a *feedback controller* is used to select appropriate actuator inputs to carry out the planned motion and correct tracking errors.

The tracking errors generated during the execution of a planned motion are due in part to the inaccuracies of the vehicle model.



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Model Predictive Control Law



The *Model Predictive Control* (MPC) model consist of a general and common methodology for autonomous vehicles control. The MPC method solves the motion planning problem over a short time horizon, by taking a short interval of the resulting open loop control and apply it to the system.

The model takes the form of a general continuous time control system with control, $u(t) \in \mathbb{R}^m$ and the state, $x(t) \in \mathbb{R}^n$.



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Pure Pursuit Control Law



The pure pursuit is a lateral control strategy. In this control law, a goal point is defined on the desired path, by looking ahead distance l_d from the current position of the rear axle center O to the desired path.

Then the curvature of the arc that connects *O* to the goal point is calculated geometrically.



Pure Pursuit Control Law



The required steering angle is calculated from the following Equation:



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Stanley Control Law



This Law was first introduced in Stanford University and won the DARPA Grand Challenge.



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Modified Sliding Control Law



The sliding mode is a robust control model and does not require a precise model of the system and can also ensure stability. The sliding surface can be defined as following:

$$\psi = k_{\theta p}\theta_p + k_d d_r$$

where the k_p and k_d are weighting coefficients. The sliding mode controller assumes that:

$$\dot{\psi} = -K_{\psi}sign(\psi)$$



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Kinematic Lateral Speed Control Law



The new *kinematic* lateral speed control designed to control the rear lateral distance and the orientation error by controlling the lateral speed d_r , which in turn is controlled by the angular speed of the car $\dot{\theta}$ through the steering angle ϕ .

As the lateral speed d_r is under control, the motions toward the path are smoother, after tuning the parameters.



Kinematic Lateral Speed Control Law



If the car is far away from the road line, it must get closer at higher speed than if it is near, so the desired lateral speed \hat{d}_r can be defined as proportional to the lateral error d_r , with negative sign.

 $\dot{d}_r = -k_{lat}d_r$

Kinematic Lateral Speed Control Law



The derivative of the lateral speed of the rear axle d_r is defined from the following Equation:





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Deep Learning models contribute to perception and to the processing of the sensory data in order to make informed decisions. The popular deep learning models used in autonomous car technology include:

End – to end Learning
Fully Convolutional Network
Deep Reinforcement Learning

CNN and Deep CNN Deep Boltzmann Machines Deep Autoencoders







Figure 19: Block diagram of and AI powered Autonomous Car.





The DNN takes as inputs the information coming from *Cameras*, *LiDAR* and *IR Sensors*.

The outputs are important information for the control of the autonomous system and concern the *Steering angle*, *Brake* and *Acceleration*.



Figure 20: A simple autonomous car DNN [TPJR18].



(VML





Deep Autonomous Control.

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The unrolled version on the right of Figure shows how the loop allows a sequence of inputs (images) to be fed to the **RNN** and the steering angle is predicted based on all those images. Specifically, the output of each layer is fed to the following layer and flow back to the previous layer.



Figure 23: RNN architecture with loops for Autonomous Driving [TPJR18].



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